

a) Assuming low speed flow, $\rho_1 \approx \rho_2 \approx \rho \rightarrow$ Bernoulli valid.

$$\therefore \rho_2 + \frac{1}{2}\rho V_2^2 = \rho_1 + \frac{1}{2}\rho V_1^2 \rightarrow \boxed{P_2 - P_1 = \frac{1}{2}\rho(V_1^2 - V_2^2)}$$

Using conditions at point 2: $\rho = \rho_2 = \frac{P_2}{RT_2} = \frac{10^5 \text{ Pa}}{287 \text{ J/kg} \cdot 300 \text{ K}} = 1.161 \text{ kg/m}^3$

$$\therefore \boxed{P_2 - P_1 = \frac{1}{2} \cdot 1.161 (10^2 - 40^2) = -871.08 \text{ Pa}}$$

$$b) \frac{P_1}{P_2} = \frac{P_2 - (P_2 - P_1)}{P_2} = \frac{100871.1}{100000} = 1.00871, \quad \boxed{P_1 = 100871.1 \text{ Pa}}$$

$$\frac{\rho_1}{\rho_2} = \left(\frac{P_1}{P_2}\right)^{\frac{1}{\gamma}} = 1.006214, \quad \boxed{\rho_1 = \rho_2 \cdot 1.006214 = 1.1682 \text{ kg/m}^3}$$

$$\frac{T_1}{T_2} = \left(\frac{P_1}{P_2}\right)^{\frac{\gamma-1}{\gamma}} = 1.00248, \quad \boxed{T_1 = T_2 \cdot 1.00248 = 300.74 \text{ K}}$$

c) $\Delta\rho/\rho = 0.00621$ i.e. 0.62% change, very small

\rightarrow so assuming $\rho \approx$ constant is reasonable

d) The mass in a soap bubble cannot change.

$$m_1 = m_2 \rightarrow \rho_1 V_1 = \rho_2 V_2, \quad \frac{V_2}{V_1} = \boxed{\frac{\rho_1}{\rho_2} = 1.00621}$$

The soap bubble expands by 0.00621, or $\boxed{+0.62\%}$

a) Total enthalpy eq'n: $\frac{Dh_0}{Dt} = \frac{1}{\rho} \frac{\partial p}{\partial t} + \dot{q} + \vec{g} \cdot \vec{V}$

Steady, adiabatic: $\frac{\partial p}{\partial t} = 0, \dot{q} = 0, \frac{\partial h_0}{\partial t} = 0$

$\therefore \frac{Dh_0}{Dt} \equiv \frac{\partial h_0}{\partial t} + \vec{V} \cdot \nabla h_0 = \vec{g} \cdot \vec{V}$ evaluate dot products

$\vec{V} \cdot \nabla h_0 = V \frac{dh_0}{dz}, \vec{g} \cdot \vec{V} = -gV$

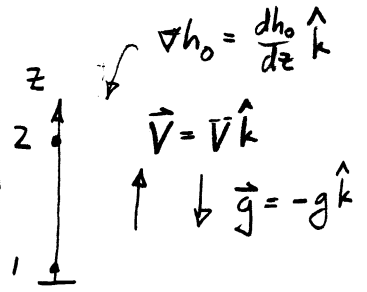
so $V \frac{dh_0}{dz} = -gV$ cancel V & integrate...

$h_0 = -gz + c \rightarrow \boxed{h_{02} - h_{01} = -g(z_2 - z_1) = -9810 \text{ m}^2/\text{s}^2}$

$h_{02} = h_2 + \frac{1}{2}V_2^2, h_{01} = h_1 + \frac{1}{2}V_1^2 \rightarrow 0$ since $V_2 = V_1 = V$

$h_2 - h_1 = h_{02} - h_{01} - \frac{1}{2}(V_2^2 - V_1^2)$

$\boxed{T_2 - T_1 = (h_2 - h_1) / c_p = -9810 \text{ m}^2/\text{s}^2 / 1004 \text{ J/kgK} = -9.77 \text{ K}}$



b) The flow is adiabatic ($\dot{q} = 0$), and reversible (no friction).

\therefore flow is isentropic.

c) Since flow is isentropic, $\frac{\rho_2}{\rho_1} = \left(\frac{T_2}{T_1}\right)^{\frac{1}{\gamma-1}}$

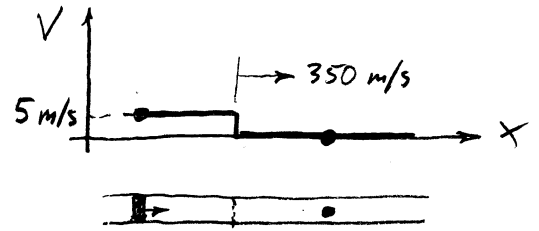
$\boxed{\frac{\rho_2}{\rho_1} = \left(\frac{T_1 + (T_2 - T_1)}{T_1}\right)^{\frac{1}{\gamma-1}} = \left(\frac{300 - 9.77}{300}\right)^{\frac{1}{\gamma-1}} = 0.9206}$

Constant mass flow: $\rho_2 V_2 A_2 = \rho_1 V_1 A_1 \rightarrow \rho_2 A_2 = \rho_1 A_1$ since $V_2 = V_1 = V$

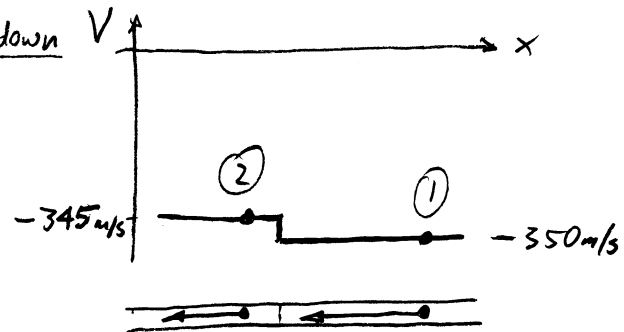
$\boxed{\frac{A_2}{A_1} = \frac{\rho_1}{\rho_2} = 1.0863}$



a) In tube's frame, air on right is still,
Air on left of shock moves with piston
at 5 m/s



In shock frame, velocities are shifted down
by shock speed $V_s = -350$ m/s



$$V_{\text{shock-frame}} = V_{\text{tube-frame}} - V_s$$

b) $h_{01} = h_1 + \frac{1}{2} V_1^2$, $h_1 = c_p T_1 = 1004 \text{ J/kg} \cdot 300 \text{ K} = 301200 \text{ m}^2/\text{s}^2$
 $\frac{1}{2} V_1^2 = \frac{1}{2} (-350 \text{ m/s})^2 = 61250 \text{ m}^2/\text{s}^2$

$\therefore h_{01} = 301200 + 61250 = 362450 \text{ m}^2/\text{s}^2$

In shock frame the flow is steady (and adiabatic) so $h_0 = \phi$

$\therefore h_{02} = h_{01} = 362450 \text{ m}^2/\text{s}^2$

c) $h_2 = h_{02} - \frac{1}{2} V_2^2 = 362450 \text{ m}^2/\text{s}^2 - \frac{1}{2} (-345 \text{ m/s})^2 = 302937.5 \text{ m}^2/\text{s}^2$

$T_2 = h_2 / c_p = 301.73 \text{ K}$

d) This is weak shock because all the changes across the shock
are small percentagewise, e.g. $|V_2 - V_1| / V_s \ll 1$, $|h_2 - h_1| / h_1 \ll 1$ etc.

e) Assuming isentropic relations are valid,

$P_2 = P_1 (T_2 / T_1)^{\frac{\gamma}{\gamma-1}} = 10^5 \text{ Pa} \cdot (301.73 / 300)^{3.5} = 10203 \text{ Pa}$

$P_2 - P_1 = 10203 - 10000 = 203 \text{ Pa}$